FIRE SAFETY REQUIREMENTS FOR DETERMINATION OF DESIGN FIRES FOR INDUSTRIAL PREMISES

FSR 4:2008

Effective Date: 25 Nov 2008

Released by:
Fire Safety Consultation Branch
Fire Safety & Shelter Department
DETERMINATION OF DESIGN FIRES
FOR INDUSTRIAL PREMISES

1. OBJECTIVE

1.1 To determine the design fire size and perimeter of fire for purpose of calculating the capacity of the natural smoke ventilation or engineered smoke control system.

2. SCOPE

2.1 This set of requirements is only applicable to sprinklered industrial premises (factory and warehouse) without in-rack sprinklers and limited to the design of smoke control system based on clause 7.6 of the Fire Code (i.e. prescriptive-based approach).

3. DETERMINATION OF DESIGN FIRE SIZE

3.1 Fire growth

3.1.1 The fire growth can be evaluated by the following generic fire growth curve (also referred to as ‘t^2 fire’), that represents the general types of combustible material present within an enclosure:

\[ Q_{\text{max}} = \propto (t-t_i)^2 \]  \hspace{1cm} \text{equation (1)}

where

- \( Q_{\text{max}} \) = heat release rate (kW);
- \( \propto \) = fire growth parameter (kJ/s^3);
- \( t \) = time (s);
- \( t_i \) = time of ignition (s) (taken here as zero)

The fire growth parameter varies with the fire load density and the fire load configuration factor. However, for purpose of design, fire growth parameter can be generally defined as follows:

<table>
<thead>
<tr>
<th>Fire growth rate</th>
<th>Fire growth parameter</th>
<th>Time for ( Q_g = 1 \text{MW} ) (s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Slow</td>
<td>0.0029</td>
<td>600</td>
</tr>
<tr>
<td>Medium</td>
<td>0.012</td>
<td>300</td>
</tr>
<tr>
<td>Fast</td>
<td>0.047</td>
<td>150</td>
</tr>
<tr>
<td>Ultra fast</td>
<td>0.188</td>
<td>75</td>
</tr>
</tbody>
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Note: Qualified Person (QP) or Fire Safety Engineer (FSE) has to justify the appropriate fire growth rate that is applicable through available literature or standard such as the SFPE Handbook. In the instance where the fire growth rate lies in between the range as stated above, the QP/FSE is to use the more conservative fire growth rate e.g. if the fire growth rate is between ‘medium’ and ‘fast’, the ‘fast’ fire growth rate is to be used.
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3.2 Design Fire - Sprinklered

3.2.1 The heat output of the design fire is assumed to increase according to equation (1) until sprinkler operation is deemed to occur at time \( t_s \). Following sprinkler operation, the heat output of the fire is considered to remain constant.

3.2.2 The capacity of the smoke control system shall be based on the fire size that is controlled by activation of 2nd ring of sprinklers.

3.2.3 The operation of the sprinkler system at \( t_s \) and the corresponding fire size can be determined by hand calculations based on fire engineering principles or the use of fire engineering tools such as FPETool from National Institute of Standards and Technology (NIST). Whichever approach is used, the following design factors governing its calculation are as follows:

a) Rate of fire growth
   The type of fuel load and its configuration in the premises shall govern the rate of fire growth which can be represented using equation (1) and table 1.

b) Sprinkler response time index (RTI)
   The RTI is the thermal sensitivity of the sprinkler and shall be based on the manufacturer’s specification.
   Example:
   Standard response sprinkler – 105 m\(^{0.5}\)\(^{0.5}\);
   Fast response sprinkler - 50m\(^{0.5}\)\(^{0.5}\);
   ESFR - 26 m\(^{0.5}\)\(^{0.5}\).

c) Temperature rating of sprinkler
   The operating temperature of the sprinklers shall be based on SS CP 52 (e.g. 141°C or 68°C).

d) Ambient temperature
   Room temperature for air-conditioned space and non-air conditioned space can be taken as 25°C and 30°C respectively.
e) Ceiling height
The ceiling height shall be based on the height, measured from the finished floor level to the soffit of the ceiling/roof.

f) Spacing of sprinkler above fire
Sprinkler spacing shall be based on SS CP 52 (e.g. 3m by 3m or 4m x 3m).

3.2.4 The capacity of the smoke control system shall also take into consideration the possibility of forklift or general goods vehicle on fire along the internal ramps/driveways. For design purpose, the design fire size shall be taken as follows:

<table>
<thead>
<tr>
<th>Type of vehicle</th>
<th>Design fire size</th>
</tr>
</thead>
<tbody>
<tr>
<td>Forklift or car</td>
<td>4MW</td>
</tr>
<tr>
<td>General goods vehicle</td>
<td>10MW</td>
</tr>
</tbody>
</table>

Table 2

4. DETERMINATION OF PERIMETER OF FIRE

4.1 Fire perimeter for forklift/car and goods vehicle

4.1.1 The fire perimeter is used to determine the mass flow rate of smoke. For forklift or general goods vehicle, the perimeter of fire shall be taken as follows:

<table>
<thead>
<tr>
<th>Type of vehicle</th>
<th>Perimeter of fire</th>
</tr>
</thead>
<tbody>
<tr>
<td>Forklift or car</td>
<td>5m x 2m</td>
</tr>
<tr>
<td>General goods vehicle</td>
<td>9m x 2.5m</td>
</tr>
</tbody>
</table>

Table 3

4.2 Fire perimeter other than for forklift/car and general goods vehicle

4.2.1 Other than for forklift/car and general goods vehicle, the following equation is used to calculate the fire perimeter for a square fire of equal sides:

\[ P = 4\left(\frac{Q_c}{Q_r}\right)^{1/2} \]  

--- equation (2)---

where

\[ P = \text{fire perimeter (m)}; \]
\[ Q_c = \text{convective heat output} = 0.7Q_{\text{max}} \text{ (kW)}; \]
\[ Q_r = \text{heat release rate per unit area (kW/m}^2) \text{, see Table 4} \]
Where elongated storage configurations such as racking or shelving are used, the fire perimeter is determined using the following equation:

\[ P = 2\left(\frac{Q_c}{(Q_r \times d)}\right) \]  \hspace{1cm} \text{equation (3)}

where

\[ Q_c = \text{convective heat output} = 0.7Q_{\text{max}} \text{ (kW)}; \]
\[ Q_r = \text{heat release rate per unit area} \text{ (kW/m}^2\text{), see Table 4; } \]
\[ d = \text{depth of rack (m)} \]

For purpose of calculating the fire perimeter, the values for \( Q_r \) given in Table 4 are used.

<table>
<thead>
<tr>
<th>Building Use</th>
<th>Heat release rate per unit area, ( Q_r ) (kW/m(^2))</th>
</tr>
</thead>
<tbody>
<tr>
<td>Industrial</td>
<td>260</td>
</tr>
<tr>
<td>Storage</td>
<td>500</td>
</tr>
</tbody>
</table>

Table 4

5. CAUTIONARY NOTE

The application of FPETool from NIST or any other software in determining the activation time of the sprinkler system and the corresponding fire size has its limitations. Some of the software programs are based on Alpert’s correlations where a number of fundamental assumptions are made such as flat smooth ceilings, unconfined smoke flow, axisymmetric plumes (not near walls or corners), location of detector close to the ceiling, etc. Such assumptions must thus be understood and considered by the user.

6. OTHER DESIGN APPROACH

The QP/FSE may adopt a different design approach using recognized standards in determining the design fire size and perimeter of fire. However, should the design approach differ from this set of guidelines, the QP/FSE is required to obtain consent from the SCDF.